# One-Shot Domain Decomposition Methods for Shape Optimization Problems

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# **1** Introduction

Shape optimization aims to optimize an objective function by changing the shape of 10 the computational domain. In recent years, shape optimization has received consid-11 erable attentions. On the theoretical side there are several publications dealing with 12 the existence of solution and the sensitivity analysis of the problem; see e.g., [6] and 13 references therein. On the practical side, optimal shape design has played an important role in many industrial applications, for example, aerodynamic shape design [7], 15 artery bypass design [1, 10], and so on. In this paper, we propose a general framework for the parallel solution of shape optimization problems, and study it in detail for the optimization of an artery bypass problem.

For PDE constrained optimization problems, there are two basic approaches: 19 nested analysis and design and simultaneous analysis and design (one-shot meth- 20 ods). As computers become more powerful in processing speed and memory capac- 21 ity, one-shot methods become more attractive due to their higher degree of paral- 22 lelism, better scalability, and robustness in convergence. The main challenges in the 23 one-shot approaches are that the nonlinear system is two to three times larger, and 24 the corresponding indefinite Jacobian system is a lot more ill-conditioned and also 25 much larger. So design a preconditioner that can substantially reduce the condition 26 number of the large fully coupled system and, at the same time, provides the scalabil- 27 ity for parallel computing becomes a very important stage in the one-shot methods. 28 There are several recent publications on one-shot methods for PDE constrained op- 29 timization problems. In [5], a reduced Hessian sequential quadratic programming 30 method was introduced for an aerodynamic design problem. In [4], a parallel *full* 31 space method was introduced for the boundary control problem where a Newton- 32 Krylov method is used together with Schur complement type preconditioners. In [9] 33 and [8], an overlapping Schwarz based Lagrange-Newton-Krylov approach (LNKSz) 34 was investigated for some boundary control problems. As far as we know no one has 35 studied shape optimization problems using LNKSz, which has the potential to solve 36 very large problems on machines with a large number of processors (np). The previ- 37

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Page 565

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ous work on LNKSz doesn't consider the change of the computational domain which 38 makes the study much more difficult and interesting. 39

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### 2 Shape Optimization on a Moving Mesh

We consider a class of shape optimization problems governed by the stationary incompressible Navier-Stokes equations defined in a two dimensional domain  $\Omega_{\alpha}$ . Our goal is to computationally find the optimal shape for part of the boundary  $\partial \Omega_{\alpha}$  such 43 that a given objective function  $J_o$  is optimized. We represent the part of the boundary 44 by a smooth function  $\alpha(x)$  determined by a set of parameters  $\mathbf{a} = (a_1, a_2, \dots, a_p)$ . By 45 changing the shape defined by  $\alpha(x)$ , one can optimize certain properties of the flow. 46 In this paper, we focus on the minimization of the energy dissipation in the whole 47 flow field and use the integral of the squared energy deformation as the objective 48 function [6]

$$\min_{\mathbf{u},\alpha} J_o(\mathbf{u},\alpha) = 2\mu \int_{\Omega_{\alpha}} \varepsilon(\mathbf{u}) : \varepsilon(\mathbf{u}) dx dy + \frac{\beta}{2} \int_{I} (\alpha'')^2 dx$$
subject to
$$\begin{cases}
-\mu \Delta \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p = \mathbf{f} \quad \text{in} \quad \Omega_{\alpha}, \\
\nabla \cdot \mathbf{u} = 0 \quad \text{in} \quad \Omega_{\alpha}, \\
\mathbf{u} = \mathbf{g} \quad \text{on} \quad \Gamma_{inlet}, \\
\mathbf{u} = \mathbf{0} \quad \text{on} \quad \Gamma_{wall}, \\
\mu \frac{\partial \mathbf{u}}{\partial \mathbf{n}} - p \cdot \mathbf{n} = \mathbf{0} \quad \text{on} \quad \Gamma_{outlet}, \\
\alpha(a) = z_1, \quad \alpha(b) = z_2,
\end{cases}$$
(1)

where  $\mathbf{u} = (u, v)$  and p represent the velocity and pressure,  $\mathbf{n}$  is the outward unit 50 normal vector on  $\partial \Omega_{\alpha}$  and  $\mu$  is the kinematic viscosity.  $\Gamma_{inlet}$ ,  $\Gamma_{outlet}$  and  $\Gamma_{wall}$  rep-51 resent the inlet, outlet and wall boundaries, respectively; see Fig. 1.  $\mathbf{f}$  is the given 52 body force and  $\mathbf{g}$  is the given velocity at the inlet  $\Gamma_{inlet}$ .  $\varepsilon(\mathbf{u}) = \frac{1}{2} (\nabla \mathbf{u} + (\nabla \mathbf{u})^T)$  is the 53 deformation tensor for the flow velocity  $\mathbf{u}$  and  $\beta$  is a nonnegative constant. I = [a, b] 54 is an interval in which the shape function  $\alpha(x)$  is defined. In the constraints, the first 55 five equations are the Navier-Stokes equations and boundary conditions and the last 56 two equations indicate that the optimized boundary should be connected to the rest 57 of the boundary and  $z_1$  and  $z_2$  are two given constants. The last term in the objective 58 function is a regularization term providing the regularity of  $\partial \Omega_{\alpha}$ .

The optimization problem (1) is discretized with a LBB-stable (*Ladyzhenskaya-* 60 *Babuška-Brezzi*)  $Q_2 - Q_1$  finite element method. Since the computational domain of 61 the problem changes during the optimization process, the mesh needs to be modified 62 following the computational domain. Generally speaking, there are two strategies to 63 modify the mesh. One is mesh reconstruction which often guarantees a good new 64 mesh but is computationally expensive. The other strategy is moving mesh which 65 is cheaper but the deformed mesh may become ill-conditioned when the boundary 66 variation is large. In our test case the boundary variations are not very large, so we 67

#### Page 566

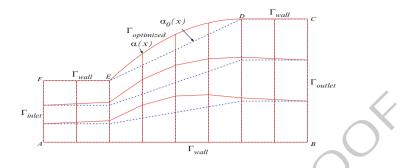


Fig. 1. The initial domain  $\Omega_{\alpha_0}$  (*dashed line*) and deformed domain  $\Omega_{\alpha}$  (*solid line*) over a simple mesh. The boundary  $\Gamma_{optimized}$  (*ED*) denotes the part of the boundary whose shape is computed by the optimization process

use the latter strategy. The moving of the mesh is simply described by Laplace's 68 equations. 69

$$\begin{cases} -\Delta \delta_{\mathbf{x}} = \mathbf{0} \quad \text{in} \quad \Omega_{\alpha_0}, \\ \delta_{\mathbf{x}} = \mathbf{g}_{\alpha} \quad \text{on} \quad \partial \Omega_{\alpha_0}, \end{cases}$$
(2)

where  $\delta_{\mathbf{x}}$  is the mesh displacement and  $\mathbf{g}_{\alpha} = (g_{\alpha}^{x}, g_{\alpha}^{y})$  is the displacement on the 70 boundary determined by  $\alpha(x)$ . Note that  $\mathbf{g}_{\alpha}$  is obtained automatically during the 71 iterative solution process. For example, in Fig. 1,  $g_{\alpha}^{x} = 0$  and  $g_{\alpha}^{y} = \alpha(x) - \alpha_{0}(x)$ . 72 The Eqs. (2) are discretized with a  $Q_{2}$  finite element method. The discretized shape 73 optimization problem is given as follows 74

$$\begin{array}{l} \min_{\mathbf{u},\mathbf{a},\delta_{\mathbf{x}}} & J_{o}(\mathbf{u},\mathbf{a},\delta_{\mathbf{x}}) = \mu \mathbf{u}^{\mathrm{T}} \mathbf{J} \mathbf{u} + \frac{\beta}{2} \mathbf{J}_{\alpha} \\ \text{subject to} \\ \begin{cases} \mathbf{K} \mathbf{u} + \mathbf{B}(\mathbf{u})\mathbf{u} - \mathbf{Q}\mathbf{p} = \mathbf{F}_{\mathbf{f}} + \mathbf{F}_{\mathbf{u}}, \\ \mathbf{Q}^{\mathrm{T}} \mathbf{u} &= \mathbf{0}, \\ \mathbf{D} \delta_{\mathbf{x}} &= \mathbf{F}_{\mathbf{x}}, \\ \mathbf{A}_{\mathbf{a}} &= \mathbf{F}_{\mathbf{a}}. \end{cases} \tag{3}$$

Here  $\mathbf{F}_{\mathbf{f}}$  refers to the discretized body force,  $\mathbf{F}_{\mathbf{u}}$  and  $\mathbf{F}_{\mathbf{x}}$  refer to the Dirichlet boundary 75 condition for  $\mathbf{u}$  and  $\delta_{\mathbf{x}}$ , respectively, and  $\mathbf{A}_{\mathbf{a}}$  and  $\mathbf{F}_{\mathbf{a}}$  are the geometric constrains. Note 76 that  $\mathbf{K}$ ,  $\mathbf{B}(\mathbf{u})$ ,  $\mathbf{Q}$  and  $\mathbf{J}$  depend on the grid displacement  $\delta_{\mathbf{x}}$ , while  $\mathbf{D}$  is independent of 77  $\delta_{\mathbf{x}}$ . Here  $\delta_{\mathbf{x}}$  is treated as an optimization variable and the moving mesh equations are 78 viewed as constraints of the optimization problem which are solved simultaneously 79 with the other equations.

# **3** One-Shot Lagrange-Newton-Krylov-Schwarz Methods

We use a Lagrange multiplier method to transform the optimization problem (3) <sup>82</sup> to a nonlinear system G(X) = 0 which is solved by an inexact Newton method. <sup>83</sup>

#### Page 567

Given an initial guess  $X^0$ , at each iteration,  $k = 0, 1, \dots$ , we use a GMRES method <sup>84</sup> to approximately solve the preconditioned system <sup>85</sup>

$$\mathbf{H}^{k}(\mathbf{M}^{k})^{-1}(\mathbf{M}^{k}\mathbf{d}^{k}) = -\mathbf{G}^{k},\tag{4}$$

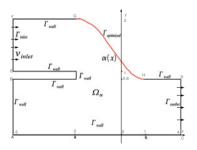
to find a search direction  $\mathbf{d}^k$ , where  $\mathbf{H}^k = \nabla_X \mathbf{G}(\mathbf{X}^k)$  is the Jacobian matrix of the <sup>86</sup> nonlinear function,  $\mathbf{G}^k = \mathbf{G}(\mathbf{X}^k)$  and  $(\mathbf{M}^k)^{-1}$  is an additive Schwarz preconditioner <sup>87</sup> [11] defined as <sup>88</sup>

$$(\mathbf{M}^k)^{-1} = \sum_{l=1}^{N_p} (R_l^\delta)^{\mathbf{T}} (\mathbf{H}_l^k)^{-1} R_l^\delta,$$

where  $\mathbf{H}_{l}^{k} = R_{l}^{\delta} \mathbf{H}^{k} (R_{l}^{\delta})^{\mathrm{T}}$ ,  $R_{l}^{\delta}$  is a restriction operator from  $\Omega_{\alpha}$  to the overlapping 90 subdomain,  $\delta$  is the size of the overlap which is understood in terms of the number 91 of elements; i.e.,  $\delta = 8$  means the overlapping size is 8 layers of elements, and  $N_{p}$  92 is the number of subdomains which is equal to np in this paper. After approximately 93 solving (4), the new approximate solution is defined as  $\mathbf{X}^{k+1} = \mathbf{X}^{k} + \tau^{k} \mathbf{d}^{k}$ , and the 94 step length  $\tau^{k}$  is selected by a cubic line search.

# **4** Numerical Experiments

The algorithm introduced in the previous sections is applicable to general shape op-97 timization problems governed by incompressible Navier-Stokes equations. Here we 98 study an application of the algorithm for the incoming part of a simplified artery by-99 pass problem<sup>1</sup> [2] as shown in Fig. 2. Our solver is implemented using PETSc [3]. 100 All computations are performed on an IBM BlueGene/L supercomputer at the Na-101 tional Center for Atmospheric Research. Unstructured meshes, which are generated 102 with CUBIT and partitioned with ParMETIS, are used in this paper.



**Fig. 2.** The incoming part of a simplified bypass model; The *red* boundary  $\Gamma_{optimized}$  denotes the part of the boundary whose shape is to be determined by the optimization process

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<sup>&</sup>lt;sup>1</sup> This is the incoming part of a bypass: www.reshealth.org/images/greystone/ em\delimiter"026E30F\_2405.gif

Without the blockage, the flow is supposed to go from AB to CD, but now we 104 assume that AB is blocked and the flow has to go through EF. For simplicity, we let 105 the thickness EF be fixed and the body force  $\mathbf{f} = \mathbf{0}$  in the Navier-Stokes equations. 106 The shape of the bypass is determined by the curve GH as in Fig. 2. The boundary 107 conditions on the inlet  $\Gamma_{intlet}$  are chosen as a constant  $v_{in}$ , no-slip boundary conditions 108 are used on the walls  $\Gamma_{wall}$ . On the outlet section  $\Gamma_{outlet}$ , the free-stress boundary 109 conditions are imposed; see (1). We use a polynomial  $\alpha(x) = \sum_{i=1}^{p} a_i x^i$  with p = 7 to 110 represent the part of the boundary that needs to be optimized. Other shape functions 111 can be used, but here we simply follow [1]. The goal is to compute the coefficients 112  $\mathbf{a} = (a_1, \dots, a_p)$ , such that the energy loss is minimized. 113

In all experiments, we use a hand-coded Jacobian matrix. The Jacobian system 114 in each Newton step is solved by a right-preconditioned restarted GMRES with an 115 absolute tolerance of  $10^{-10}$ , a relative tolerance of  $10^{-3}$ , and a restart at 100. We stop 116 the Newton iteration when the nonlinear residual is decreased by a factor of  $10^{-6}$ .

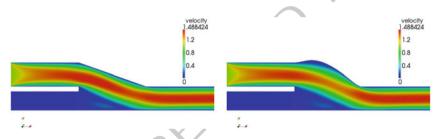


Fig. 3. Velocity distribution of the initial (*left*) and optimal shapes (*right*). The initial shape is given by a *straight line*.  $\beta = 0.01$  and Re = 100

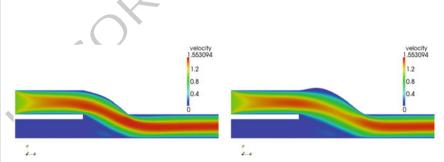


Fig. 4. Velocity distribution of the initial (*left*) and optimal shapes (*right*). The initial shape is given as  $\alpha(x) = 0.4 + 0.45x^2 + 0.15x^3$ .  $\beta = 0.01$  and Re = 100

In the first test case, we set the Reynolds number  $Re = \frac{Lv_{in}}{\mu}$  to 100, where  $L = \frac{11}{118}$ 1.0 cm is the artery diameter,  $v_{in} = 1.0$  cm/s is the inlet velocity and  $\mu = 0.01$  cm<sup>2</sup>/s. 119

#### Page 569

We solve the problem on a mesh with about 18,000 elements.  $\beta = 0.01$  and the degrees of freedom (DOF) is 589,652. The initial shape is given by a straight line, and 121 Fig. 3 shows the velocity distribution of the initial (left) and optimal shapes (right). 122 The energy dissipation of the optimized shape is reduced by about 5.13 % compared 123 to the initial shape. Figure 4 is the velocity distribution of another initial shape (left) 124 which is given as  $\alpha(x) = 0.4 + 0.45x^2 + 0.15x^3$  and the corresponding optimal shape 125 (right). The reduction of the energy dissipation of this case is about 11.96%. Figures 3 and 4 show that we can obtain nearly the same optimal shape from different 127 initial shapes. 128

In the test case showed in Fig. 3, if we add a small inlet velocity at the boundary 129 AB, which is equal to that the blood flow is not totally blocked, the computed optimal 130 shape would be different from what is shown in Fig. 3. If we move the boundary 131 AB towards CD (A from (-5,0) to (-3,0) and B from (-5,0.8) to (-3,0.8)), the 132 optimal shape is nearly the same as Fig. 3 since the flow in the "dead area" doesn't 133 impact much of the optimal solution.

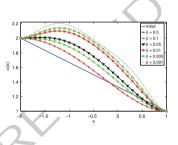


Fig. 5. The initial shape and optimal shapes with different values of parameter  $\beta$ . DOF = 589,652 and Re = 100

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The regularization parameter  $\beta$  in the objective function is very important for 135 shape optimization problems. From Table 1 we see that reducing  $\beta$  can increase the 136 reduction of the energy dissipation ("Init.", "Opt." and "Reduction" are the initial, 137 optimized and reduction of the energy dissipation in the table), but the number of 138 Newton (Newton) and the average number of GMRES iterations per Newton (GM-139 RES) and the total compute time in seconds (Time) increase, which means that the 140 nonlinear algebraic system is harder to solve when  $\beta$  is small. This is because the 141 boundary of  $\Omega_{\alpha}$  is more flexible and may become irregular when  $\beta$  is too small. Fig-142 ure 5 shows the initial shape and the optimized shapes obtained with different values 143 of  $\beta$ . From this figure we see that  $\beta$  controls the boundary deformation. 144

To show the parallel scalability of the algorithm, two meshes with DOF = 145589,652 and DOF = 928,572 are considered. The strong scalability of our algorithm 146 is good; see Fig. 6 and Table 2, which show that the speedup is almost linear when 147 *np* is small. As expected in one-level Schwarz methods, the preconditioner becomes 148 worse as the number of subdomains increases. 149

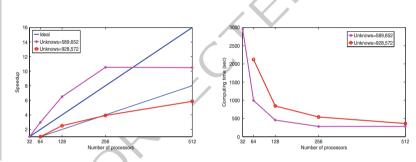
Table 3 shows some results for different *Re*. Judging from the increase of the 150 number of linear and nonlinear iterations, it is clear that the problem becomes harder 151

β	Newton	GMRES	Time	Energy Dissipation		
β	inewion	UNIKES	Time	Init.	Opt.	Reduction
0.05	4					4.27%
0.01	5	441.40	600.86	1.17	1.11	5.13%
0.005	5	439.00	599.77	1.17	1.10	5.98%
0.001	6	510.67	747.78	1.17	1.10	5.98%

**Table 1.** Effect of the parameter  $\beta$ . *DOF* = 589,652, *Re* = 100.

**Table 2.** Parallel scalability for two different size grids.  $\beta = 0.1$ , overlap = 6 and Re = 100.

				-		
np	DOF = 589,652			DOF = 928,572		
	Newton	GMRES	Time	Newton	GMRES	Time
32	4	124.50	2959.73			
64	4	179.25	980.48	4	146.50	2121.52
128	4	346.75	455.69	4	330.00	844.62
256	4	533.25	280.96	4	520.75	541.97
512	4	917.50	282.07	4	861.00	361.08



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Fig. 6. The speedup and the total compute time for two different mesh sizes. Re = 100

as we increase the *Re*. On the other hand, we achieve higher percentage of reduction <sup>152</sup> of energy dissipation in the harder to solve situations.

**Table 3.** The impact of *Re*.  $\beta = 0.1$ , *overlap* = 8, *DOF* = 589,652, *np* = 128.

D	Newton GMRES	m.	Energy Dissipation				
	Re	Newton	GMRES	Time	Init.	Opt.	Reduction
	100	4	346.75	456.83	1.17	1.13	3.42%
	200	4	372.00	470.16	0.65	0.62	4.62%
	300	6		871.19			
	600	7	721.71	1035.84	7.43	6.97	6.19%

## **5** Conclusions and Future Work

We developed a parallel one-shot LNKSz for two-dimensional shape optimization 155 problems governed by incompressible Navier-Stokes equations. We tested the algorithms for an artery bypass design problem with more than 900,000 DOF and up to 512 processors. The numerical results show that our method is quite robust with respect to the *Re* and the regularization parameter. The strong scalability is almost ideal 159 when *np* is not too large. In the future, we plan to study some multilevel Schwarz 160 methods which may improve the scalability when *np* is large. 161

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